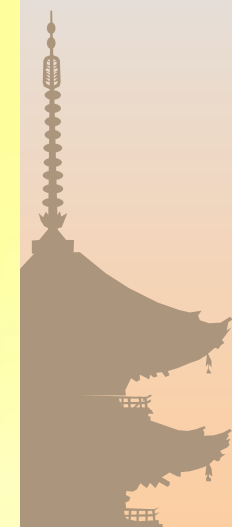
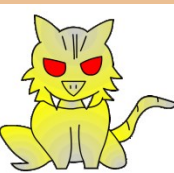




輻射性衝撃波の構造

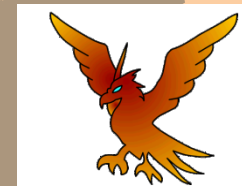
Radiative Shocks





目次

- 1 輻射性衝撃波の概要
- 2 平衡拡散近似での解: ガス圧優勢、輻射圧優勢
- 3 相対論的輻射性衝撃波
- 4 円盤降着流における輻射性衝撃波
- 5 今後の課題





概要

❁ 構造

- 前駆領域 precursor
- 緩和領域 relaxation

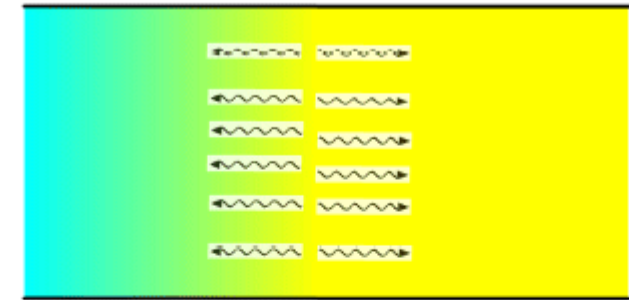
今回

❁ 分類(光学の厚み)

- thick-thick
- thin-thin
- thin-thick
- thick-thin △

今回

radiation transport



r_s

pre-shock 1

post-shock 2

radiative precursor

ρ

v

r_s





概要

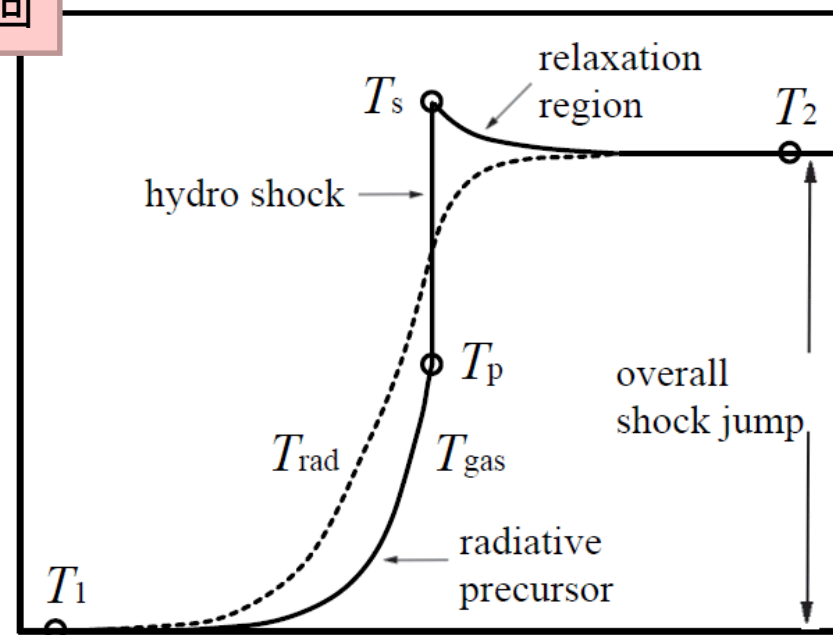
❁ 分類(ガス輻射平衡)

- strong equilibrium limit
(1流体近似) 有効比熱比 Γ
- equilibrium diffusion app.
($T_{\text{rad}} = T_{\text{gas}}$)
- nonequilibrium diffusion
($T_{\text{rad}} < T_{\text{gas}}$)

$$\Gamma \equiv \frac{\beta + (\gamma - 1)(4 - 3\beta)}{\beta + 3(\gamma - 1)(1 - \beta)}.$$

□ 分類(M1, 温度分布)

- subcritical ($T_p < T_2$)
- critical ($T_p = T_2$)
- supercritical ($T_p > T_2$)





平衡拡散近似

- ❁ 構造方程式

衝撃波上流 2、無印

衝撃波下流 1

- ❁ 衝撃波座標 x

- ❁ 密度 ρ

- ❁ 相対速度 u

- ❁ ガス圧、輻射圧 p, P

- ❁ 内部E e, E

- ❁ 温度、輻射流束 T, F

$$\rho u = \rho_1 u_1 = j, \quad (23.73)$$

$$\rho u^2 + p + P = \rho_1 u_1^2 + p_1 + P_1, \quad (23.74)$$

$$u \left(\frac{1}{2} \rho u^2 + e + p + E + P \right) + F = u_1 \left(\frac{1}{2} \rho_1 u_1^2 + e_1 + p_1 + E_1 + P_1 \right), \quad (23.75)$$

$$F = -\frac{c}{\kappa \rho} \frac{dP}{dx} = -\frac{4acT^3}{3\kappa \rho} \frac{dT}{dx}, \quad (23.76)$$



平衡拡散近似

- ❁ 跳び条件→
- ❁ RH関係↓

$$\begin{aligned}\rho_2 u_2 &= \rho_1 u_1 = j, \\ \rho_2 u_2^2 + p_2 + P_2 &= \rho_1 u_1^2 + p_1 + P_1, \\ \frac{1}{2} u_2^2 + \frac{\gamma}{\gamma - 1} \frac{p_2}{\rho_2} + \frac{4P_2}{\rho_2} &= \frac{1}{2} u_1^2 + \frac{\gamma}{\gamma - 1} \frac{p_1}{\rho_1} + \frac{4P_1}{\rho_1},\end{aligned}$$

$$\begin{aligned}\frac{\gamma}{\gamma - 1} \frac{p_2}{\rho_2} + \frac{4P_2}{\rho_2} - \left(\frac{\gamma}{\gamma - 1} \frac{p_1}{\rho_1} + \frac{4P_1}{\rho_1} \right) \\ - \frac{1}{2} [p_2 + P_2 - (p_1 + P_1)] \left(\frac{1}{\rho_1} + \frac{1}{\rho_2} \right) = 0,\end{aligned}\quad (23.80)$$

$$\frac{p_2 + P_2 - (p_1 + P_1)}{\rho_2 - \rho_1} = \frac{\rho_1}{\rho_2} a_1^2 \mathcal{M}_1^2 = \frac{1}{\rho_2} \gamma p_1 \mathcal{M}_1^2,\quad (23.81)$$

where $a_1 (\equiv \sqrt{\gamma p_1 / \rho_1})$ is the sound speed in the upstream region, and $\mathcal{M}_1 (\equiv u_1 / a_1)$ the Mach number of the upstream flow.

温度に関する9次方程式→ガス圧優勢 or 輻射圧優勢

2019/8/10

ASJ Meeting 2018





平衡拡散近似

✿ 前駆領域 (衝撃波座標 x)

$$\frac{4acT^3}{3\kappa\rho} \frac{dT}{dx} = \left(\frac{1}{2}\rho u^2 + \frac{\gamma}{\gamma-1}p + 4P \right) u - \left(\frac{1}{2}\rho_1 u_1^2 + \frac{\gamma}{\gamma-1}p_1 + 4P_1 \right) u_1. \quad (23.82)$$

Eliminating u ($= \rho_1 u_1 / \rho$), and again introducing the Mach number $\mathcal{M}_1$ ($= u_1/a_1$) in the upstream region, we can arrange the above equation as

$$\frac{4acT^3}{3\kappa\rho} \frac{dT}{dx} = \left\{ \frac{1}{2} \frac{\gamma p_1}{\rho_1} \mathcal{M}_1^2 \left[\left(\frac{\rho_1}{\rho} \right)^2 - 1 \right] + \frac{\gamma}{\gamma-1} \left(\frac{p}{\rho} - \frac{p_1}{\rho_1} \right) + \frac{4P}{\rho} - \frac{4P_1}{\rho_1} \right\} \rho_1 u_1. \quad (23.83)$$

Similarly, the momentum conservation (23.74) is rearranged as

$$p - p_1 = \rho_1 a_1^2 \mathcal{M}_1^2 \left(1 - \frac{\rho_1}{\rho} \right) - (P - P_1). \quad (23.84)$$





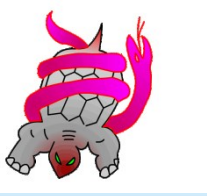
平衡拡散近似

❁ 前駆領域(つづき)

Substituting equations of state $p = (\mathcal{R}/\mu)\rho T$ and $P = aT^4/3$ into equations (23.83) and (23.84), we have two equations on the two variables (ρ and T):

$$\begin{aligned} \frac{4acT^3}{3\kappa\rho} \frac{dT}{dx} = & \left\{ \frac{1}{2}\gamma \frac{\mathcal{R}}{\mu} T_1 \mathcal{M}_1^2 \left[\left(\frac{\rho_1}{\rho} \right)^2 - 1 \right] + \frac{\gamma}{\gamma-1} \frac{\mathcal{R}}{\mu} T_1 \left(\frac{T}{T_1} - 1 \right) \right. \\ & \left. + \frac{1}{\rho_1} \frac{4}{3} a T_1^4 \left[\frac{\rho_1}{\rho} \left(\frac{T}{T_1} \right)^4 - 1 \right] \right\} \rho_1 u_1, \end{aligned} \quad (23.85)$$

$$\frac{\mathcal{R}}{\mu} \rho_1 T_1 \left(\frac{\rho}{\rho_1} \frac{T}{T_1} - 1 \right) = \gamma \frac{\mathcal{R}}{\mu} \rho_1 T_1 \mathcal{M}_1^2 \left(1 - \frac{\rho_1}{\rho} \right) - \frac{a}{3} T_1^4 \left[\left(\frac{T}{T_1} \right)^4 - 1 \right]. \quad (23.86)$$



平衡拡散近似

❁ 前駆領域(つづき)

Introducing the nondimensional quantities, $\tilde{\rho}$ ($\equiv \rho/\rho_1$), $\tilde{T}$ ($\equiv T/T_1$) and $\tilde{x}$ ($\equiv x/\ell_1$, ℓ_1 being a typical length scale), we can finally express equations (23.85) and (23.86), respectively, as

$$\frac{4\alpha_1}{\beta_1\tau_1} \frac{\tilde{T}^3}{\tilde{\rho}} \frac{d\tilde{T}}{d\tilde{x}} = \frac{\gamma}{2} \mathcal{M}_1^2 \left(\frac{1}{\tilde{\rho}^2} - 1 \right) + \frac{\gamma}{\gamma-1} (\tilde{T} - 1) + 4\alpha_1 \left(\frac{\tilde{T}^4}{\tilde{\rho}} - 1 \right) \quad (23.87)$$

$$\tilde{\rho} = \frac{1 + \gamma \mathcal{M}_1^2 - \alpha_1(\tilde{T}^4 - 1) - \sqrt{[1 + \gamma \mathcal{M}_1^2 - \alpha_1(\tilde{T}^4 - 1)]^2 - 4\gamma \mathcal{M}_1^2 \tilde{T}}}{2\tilde{T}}, \quad (23.88)$$

where α_1 ($\equiv P_1/p_1$), β_1 ($\equiv u_1/c$), and τ_1 ($\equiv \kappa\rho_1\ell_1$). From the physical viewpoints, we here separate several parameters, although β_1 and τ_1 can be renormalized in the coordinate scale. In addition, the root for $\tilde{\rho}$ was chosen so as to $\tilde{\rho}(\tilde{T}_1) = 1$.



平衡拡散近似 ガス圧優勢

❁ 跳び条件と前駆領域の構造方程式

$$\tilde{\rho}_2 \equiv \frac{\rho_2}{\rho_1} = \frac{(\gamma + 1)\mathcal{M}_1^2}{(\gamma - 1)\mathcal{M}_1^2 + 2}, \quad (23.89)$$

$$\tilde{p}_2 \equiv \frac{p_2}{p_1} = \frac{2\gamma\mathcal{M}_1^2 - (\gamma - 1)}{\gamma + 1}, \quad (23.90)$$

$$\tilde{T}_2 \equiv \frac{T_2}{T_1} = \frac{[2\gamma\mathcal{M}_1^2 - (\gamma - 1)][(\gamma - 1)\mathcal{M}_1^2 + 2]}{(\gamma + 1)^2\mathcal{M}_1^2}. \quad (23.91)$$

$$\frac{4\alpha_1}{\beta_1\tau_1} \frac{\tilde{T}^3}{\tilde{\rho}} \frac{d\tilde{T}}{d\tilde{x}} = \frac{\gamma}{2}\mathcal{M}_1^2 \left(\frac{1}{\tilde{\rho}^2} - 1 \right) + \frac{\gamma}{\gamma - 1} (\tilde{T} - 1), \quad (23.92)$$

$$\tilde{\rho} = \frac{1 + \gamma\mathcal{M}_1^2 - \sqrt{(1 + \gamma\mathcal{M}_1^2)^2 - 4\gamma\mathcal{M}_1^2\tilde{T}}}{2\tilde{T}}, \quad (23.93)$$



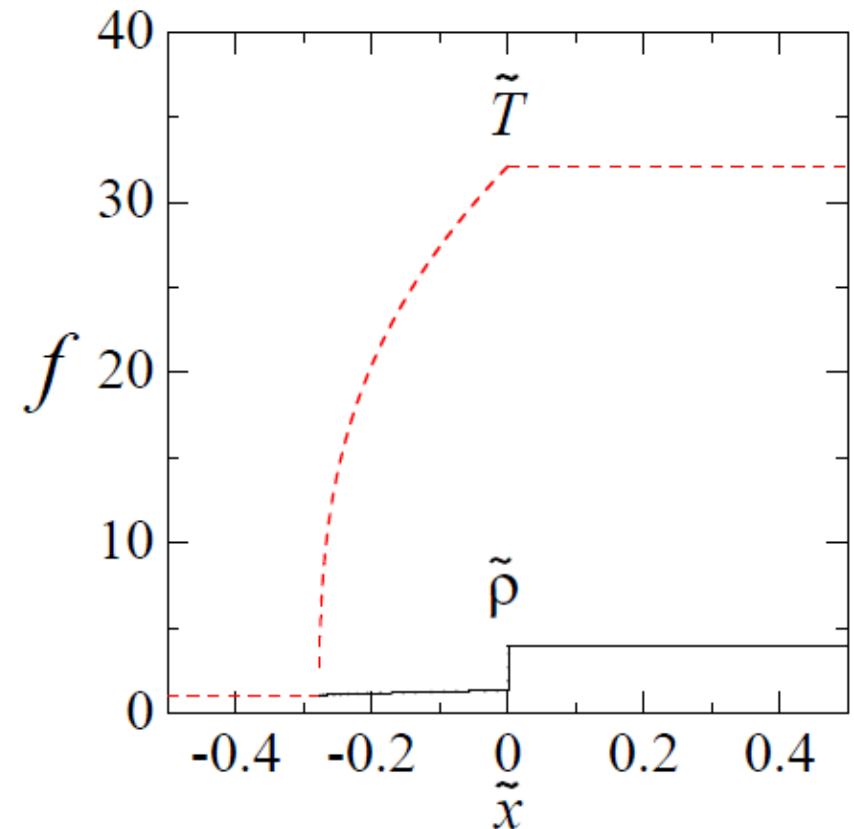


平衡拡散近似 ガス圧優勢

- 密度構造は不連続
- 温度構造は連続
- isothermal shock

- 輻射性衝撃波では輻射エネルギーが上流へ貫入し、前駆領域の温度を上昇させる。ガス圧優勢の場合、衝撃波が強くなると、上流の温度は急激に上昇し、下流の温度に達する。下流の温度より高くはなれないので、その後は、前駆領域を押し広げていく。

- $\gamma=5/3; \alpha_1/\beta_1\tau_1=0.00001;$
 $M_1=10$





平衡拡散近似 輻射圧優勢

❁ 跳び条件と前駆領域の構造方程式

$$\frac{4P_2}{\rho_2} - \frac{4P_1}{\rho_1} - \frac{1}{2} (P_2 - P_1) \left(\frac{1}{\rho_1} + \frac{1}{\rho_2} \right) = 0, \quad (23.98)$$

$$\frac{P_2 - P_1}{\rho_2 - \rho_1} = \frac{\rho_1}{\rho_2} a_1^2 \mathcal{M}_1^2 = \frac{P_1}{\rho_1} \frac{\gamma}{\alpha_1} \mathcal{M}_1^2, \quad (23.99)$$

which are easily solve to yield

$$\tilde{\rho}_2 \equiv \frac{\rho_2}{\rho_1} = \frac{7\gamma\mathcal{M}_1^2/\alpha_1}{\gamma\mathcal{M}_1^2/\alpha_1 + 8}, \quad (23.100)$$

$$\tilde{P}_2 \equiv \frac{P_2}{P_1} = \frac{6\gamma\mathcal{M}_1^2/\alpha_1 - 1}{7}. \quad (23.101)$$

$$\frac{1}{\beta_1\tau_1} \frac{1}{\tilde{\rho}} \frac{d\tilde{P}}{d\tilde{x}} = \frac{1}{2} \frac{\gamma}{\alpha_1} \mathcal{M}_1^2 \left(\frac{1}{\tilde{\rho}^2} - 1 \right) + 4 \left(\frac{\tilde{P}}{\tilde{\rho}} - 1 \right), \quad (23.102)$$

$$\frac{1}{\tilde{\rho}} = 1 + \frac{1 - \tilde{P}}{\gamma\mathcal{M}_1^2/\alpha_1}. \quad (23.103)$$





平衡拡散近似 輻射圧優勢



- 密度構造が連続

- continuous shock

- 輻射圧優勢の場合、衝撃波が強くなっても、上流の温度はそれほど上昇しないが、密度構造は連続的に変化。

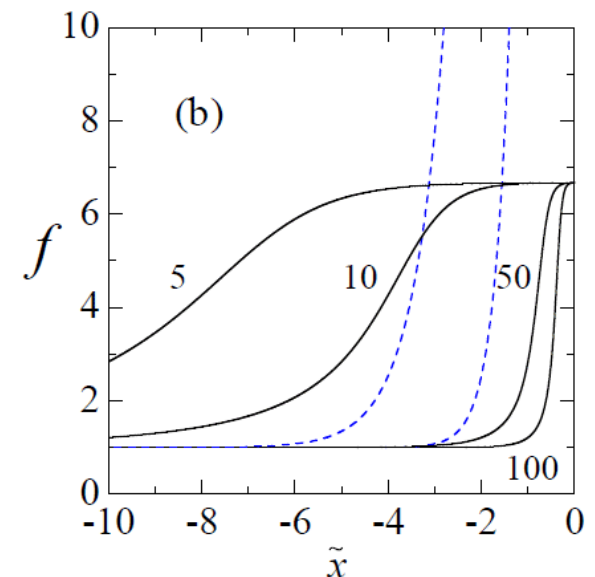
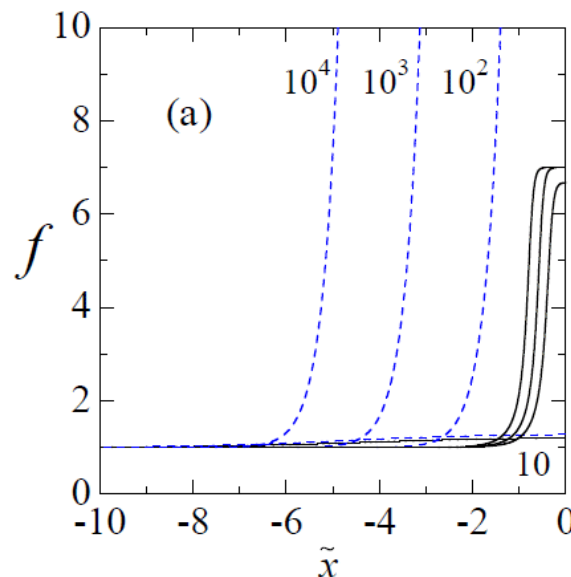
- 圧縮率は
最大7倍

- $\gamma=5/3; \alpha_1=100; \beta_1=0.01$

- (a) $\tau_1=100; M_1=10^{-4}$

- (b) $M_1=100; \tau_1=5-100$

- 実線 ρ 、破線 P

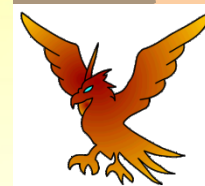
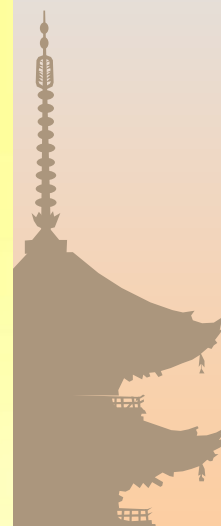




相對論的輻射性衝擊波

Fukue 2019b

福江 純 @ 大阪教育大学



相対論的輻射性衝撃波 ガス圧優勢

❁ 跳び条件

❁ $\Gamma = 5/3$

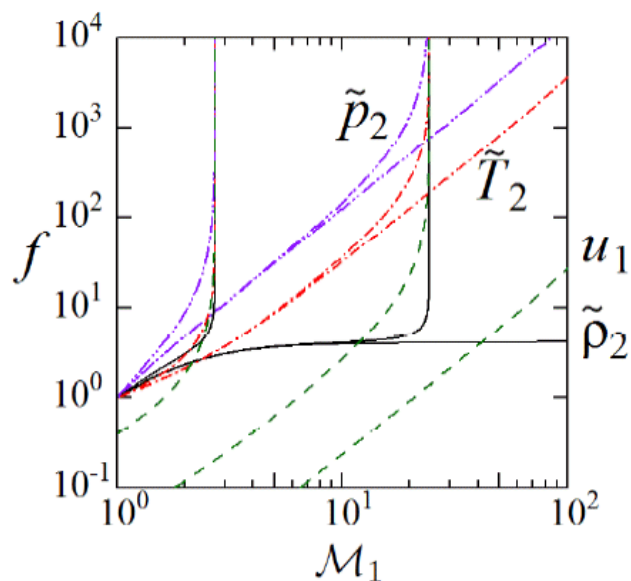


Fig. 25.2 Post-shock quantities as a function of $\mathcal{M}_1$ in the gas-pressure dominated case ($\Gamma = 5/3$). Solid curves represent $\tilde{p}_2$, where $\nu_1 = 0.00001, 0.001, 0.1$ from right to left. Chain-dotted ones mean $\tilde{T}_2$, where $\nu_1 = 0.00001, 0.001, 0.1$ from right to left, while two-dot chain ones are $\tilde{\rho}_2$, where $\nu_1 = 0.00001, 0.001, 0.1$ from right to left. Finally, dashed ones denote the pre-shock u_1 , where $\nu_1 = 0.00001, 0.001, 0.1$ from bottom to top.



相對論的輻射性衝擊波 ガス圧優勢



❁ 前駆領域

❁ $\Gamma=5/3$

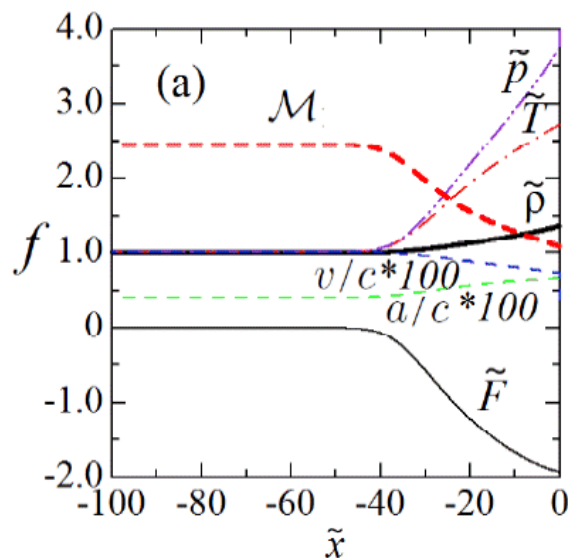


Fig. 25.4 Typical solutions for the radiative precursor region of the relativistic radiative shocks in the gas-pressure dominated case as a function of the normalized coordinate. Thick solid curves represent $\tilde{\rho}$, thin chain-dotted ones $\tilde{T}$, thin two-dot chain ones $\tilde{p}$, thin dashed ones v/c (upper) and a/c , thick dashed ones $\mathcal{M}$, and thin solid ones $\tilde{F}$. The parameters are $\Gamma = 5/3$ and (a) $\nu_1 = 0.00001$ and $\mathcal{M}_1 = 2.46$ ($\tilde{p}_2 = 7.3$, $\beta_1 = 0.01$), and (b) $\nu_1 = 0.1$ and $\mathcal{M}_1 = 2.20$ ($\tilde{p}_2 = 9.3$, $\beta_1 = 0.74$). The density distribution is discontinuous, while the temperature one is continuous.



相対論的輻射性衝撃波

輻射圧優勢

❁ 跳び条件

❁ $\Gamma = 5/3$

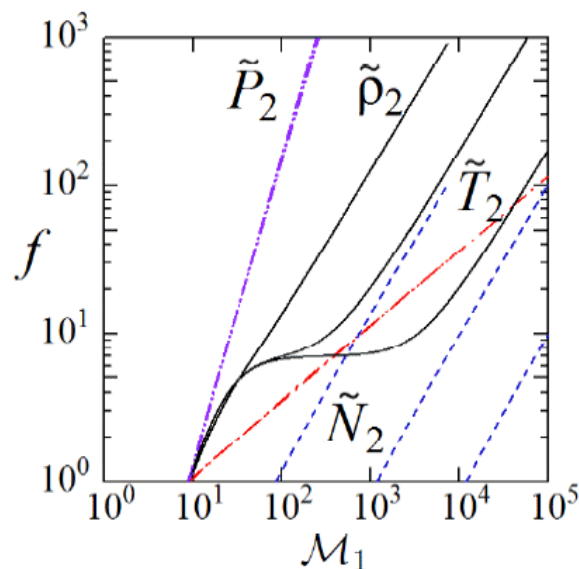


Fig. 25.6 Post-shock quantities as a function of $\mathcal{M}_1$ in the radiation-pressure dominated case. Solid curves represent $\tilde{\rho}_2$, where $\nu_1 = 0.00001, 0.001, 0.1$ from right to left. Chain-dotted ones mean $\tilde{T}_2$, while two-dot chain ones are $\tilde{P}_2$; both do not depend on N_2 . Finally, dashed ones denote N_2 , where $N_1 = 0.00001, 0.001, 0.1$ from right to left. The parameters are $\Gamma = 5/3$ and $\alpha_1 = 100$.



相對論的輻射性衝擊波

輻射壓優勢



❁ 前驅領域

❁ $\Gamma=5/3$

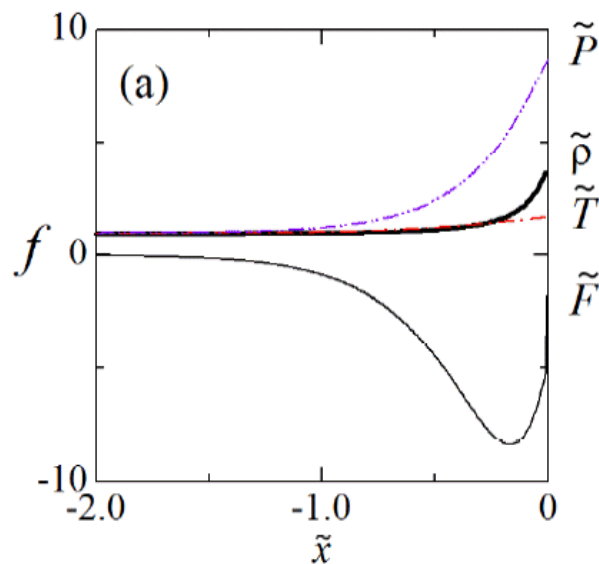


Fig. 25.8 Typical solutions for the radiative precursor region of the relativistic radiative shocks in the radiation-pressure dominated case as a function of the normalized coordinate. Thick solid curves represent $\tilde{\rho}$, thin chain-dotted ones $\tilde{T}$, thin two-dot chain ones $\tilde{P}$, and thin solid ones $\tilde{F}$. The parameters are $\Gamma = 5/3$ and $\alpha_1 = 100$ (a) $N_1 = 0.00001$ and $\mathcal{M}_1 = 24.8$ ($N_2 = 0.000022$, $\beta_1 = 0.01$), and (b) $N_1 = 0.1$ and $\mathcal{M}_1 = 52.85$ ($N_2 = 0.55$, $\beta_1 = 0.91$). The temperature distribution is continuous.





円盤降着流における 輻射性衝撃波の構造

Fukue 2019a

Radiative Shocks in Disk Accretion

福江 純 @ 大阪教育大学



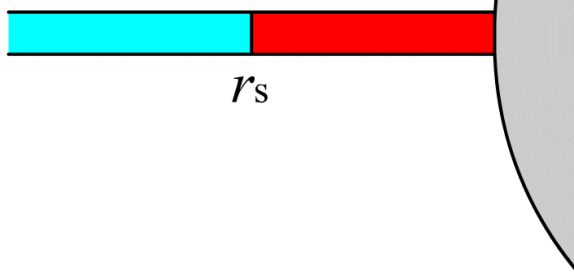


円盤降着と輻射性衝撃波

HD: 1D hydro shocks

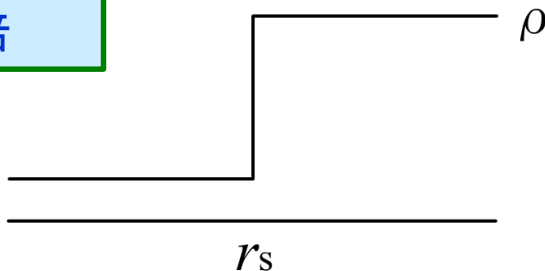
(a)

不連続
厚み一定



1 2

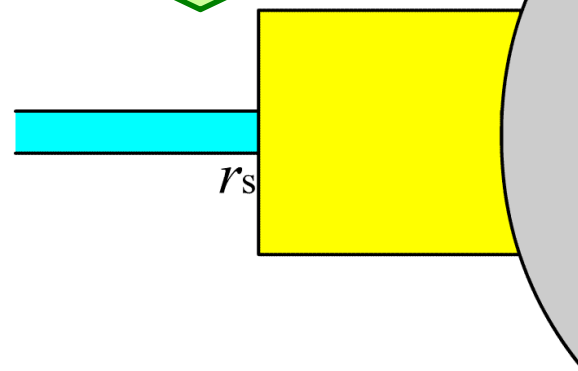
密度 ρ
最大4倍



HD: vertical

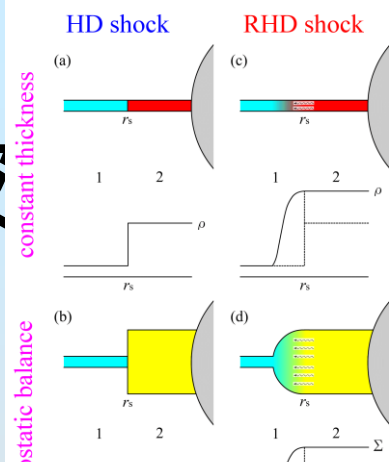
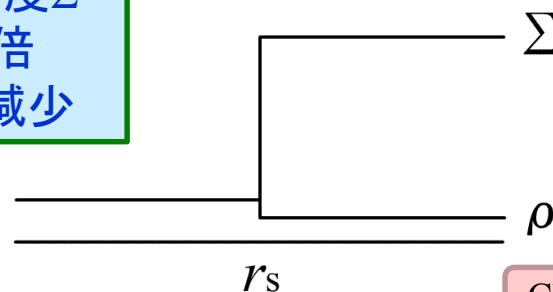
(b)

不連続
膨らむ



1 2

表面密度 Σ
最大4倍
密度 ρ 減少



Fukue 1987

J Meeting 2

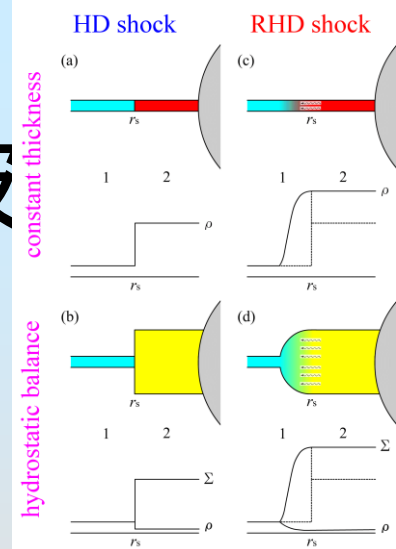


Chakrabarti 1989



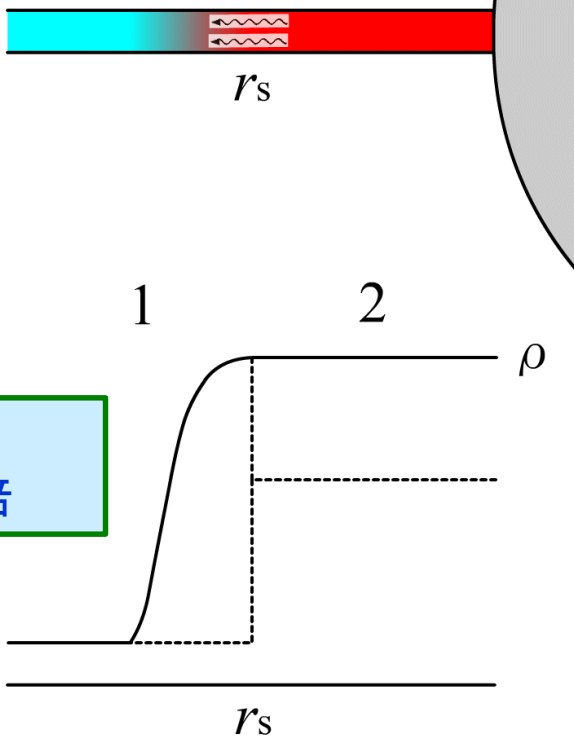
円盤降着と輻射性衝撃波

❁ RHD: 1D radiative shocks



(c)

連続的变化
厚み一定



密度 ρ
最大7倍

- ❁ (光学的に厚い)
- ❁ 輻射拡散の効果

Zel'dovich 1957
Raizer 1957
Zel'dovich+Raizer 1966
Mihalas+Mihalas 1984
Lacey 1988
Bouquet+ 2000
Drake 2005, 2007
Lowrie+ 1999
Lowrie+Rauenzahn 2007
Lowrie+Edwards 2008
Tolstov+ 2015
Ferguson+ 2017



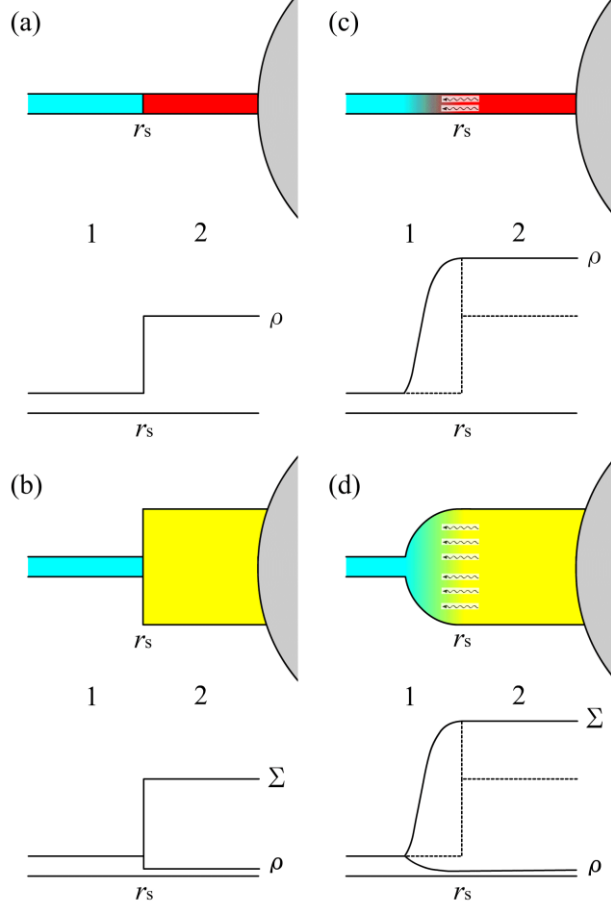


円盤降着と輻射性衝撃波

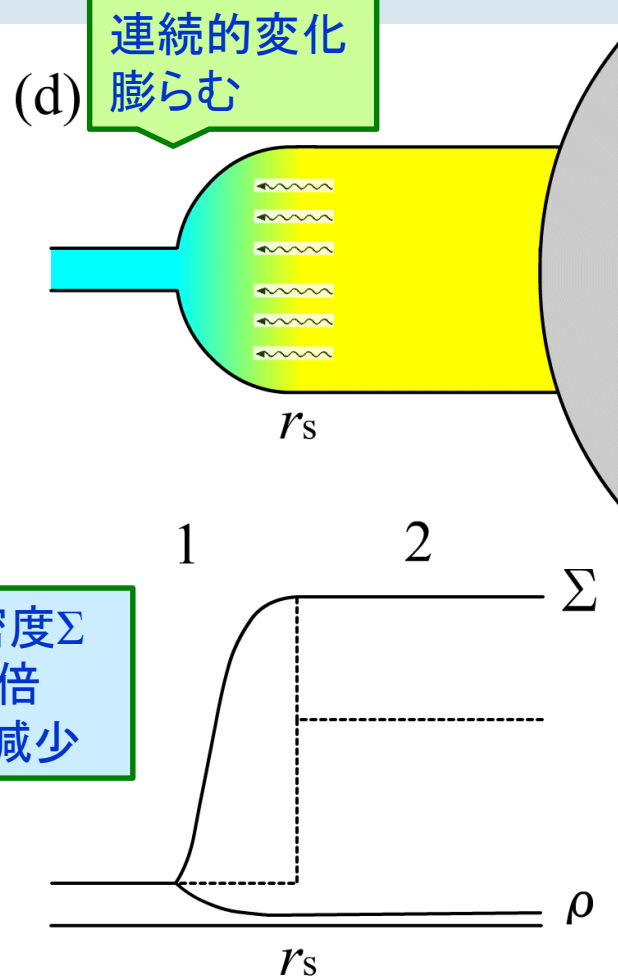
❁ RHD: radiative/vertical

HD shock

RHD shock



輻射拡散
静水圧平衡

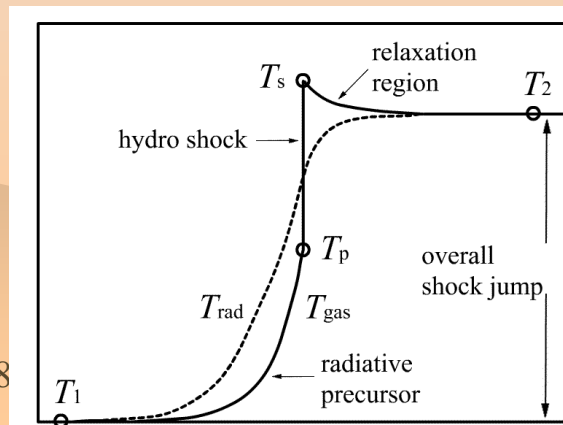


表面密度 Σ
最大7倍
密度 ρ 減少

2 基礎方程式：平衡拡散近似

- ❁ 半径方向の降着流
- ❁ 光学的に厚い
- ❁ 平衡拡散近似
- ❁ エディントン近似
- ❁ 鉛直方向静水圧平衡
- ❁ 重力場・角運動量無視

- ❁ Strong Equilibrium
 - 有効比熱比
- ❁ Equilibrium Diffusion Approximation
 - $T_{\text{rad}} = T_{\text{gas}}$
 - 輻射拡散
- ❁ Nonequilibrium Diff.



- $T_{\text{rad}} \neq T_{\text{gas}}$
- ゼルドヴィッチスパイク

2 基礎方程式：平衡拡散近似

- mass flux
- momentum flux
- energy flux
- radiative diffusion
- vertical hydrostatic

$$\begin{aligned} h\rho u &= h_1\rho_1 u_1 = j \text{ (constant),} \\ h(\rho u^2 + p + P) &= h_1(\rho_1 u_1^2 + p_1 + P_1) \\ h\rho u \left(\frac{1}{2}u^2 + \frac{\gamma}{\gamma-1}\frac{p}{\rho} + \frac{4P}{\rho} \right) + hF &= \\ h_1\rho_1 u_1 \left(\frac{1}{2}u_1^2 + \frac{\gamma}{\gamma-1}\frac{p_1}{\rho_1} + \frac{4P_1}{\rho_1} \right), \end{aligned}$$

$$F = -\frac{c}{\kappa\rho} \frac{dP}{dx} = -\frac{4acT^3}{3\kappa\rho} \frac{dT}{dx},$$

$$\begin{aligned} \frac{GM}{r^3} h^2 &= \frac{p+P}{\rho}, \\ \frac{GM}{r_1^3} h_1^2 &= \frac{p_1+P_1}{\rho_1}, \end{aligned}$$

or combined into the form:

$$h^2 \frac{\rho}{p+P} = h_1^2 \frac{\rho_1}{p_1+P_1},$$

2 基礎方程式：平衡拡散近似

- overall jump conditions
- 密度 ρ
- 速度 u
- 拡散項は落とす
- ガス圧 p , 輻射圧 P
- 厚み h

$$\begin{aligned}h_2 \rho_2 u_2 &= h_1 \rho_1 u_1 = j, \\h_2 (\rho_2 u_2^2 + p_2 + P_2) &= h_1 (\rho_1 u_1^2 + p_1 + P_1), \\ \frac{1}{2} u_2^2 + \frac{\gamma}{\gamma - 1} \frac{p_2}{\rho_2} + \frac{4P_2}{\rho_2} &= \frac{1}{2} u_1^2 + \frac{\gamma}{\gamma - 1} \frac{p_1}{\rho_1} + \frac{4P_1}{\rho_1}, \\ \frac{h_2^2}{h_1^2} &= \frac{\rho_1}{\rho_2} \frac{p_2 + P_2}{p_1 + P_1}\end{aligned}$$

2 基礎方程式：平衡拡散近似

Rankine-Hugoniot relation

$$\begin{aligned} & \frac{\gamma}{\gamma-1} \frac{p_2}{\rho_2} + \frac{4P_2}{\rho_2} - \left(\frac{\gamma}{\gamma-1} \frac{p_1}{\rho_1} + \frac{4P_1}{\rho_1} \right) \\ & + \frac{1}{2} \frac{\frac{h_2}{h_1} (p_2 + P_2) - (p_1 + P_1)}{\frac{h_2}{h_1} \rho_2 - \rho_1} \left(\frac{\rho_1}{\rho_2} \frac{h_1}{h_2} - \frac{\rho_2}{\rho_1} \frac{h_2}{h_1} \right) = 0, \quad (12) \\ & \left[\frac{h_2}{h_1} (p_2 + P_2) - (p_1 + P_1) \right] \frac{\frac{h_2}{h_1} \rho_2}{\frac{h_2}{h_1} \rho_2 - \rho_1} = \gamma p_1 \mathcal{M}_1^2 \end{aligned}$$

where $\mathcal{M}_1$ ($\equiv u_1/a_1$) the Mach number of the upstream flow,

$$\left(\frac{h_2}{h_1} \right)^2 = \frac{\rho_1}{\rho_2} \frac{p_2 + P_2}{p_1 + P_1}.$$

2 基礎方程式：平衡拡散近似

❁ Radiative Precursor

❁ 温度 T : 衝撃波座標 x

$$\begin{aligned} h \frac{c}{\kappa \rho} \frac{dP}{dx} &= h \frac{4acT^3}{3\kappa\rho} \frac{dT}{dx} \\ &= \left(\frac{1}{2}u^2 + \frac{\gamma}{\gamma-1} \frac{p}{\rho} + \frac{4P}{\rho} \right) h\rho u \\ &\quad - \left(\frac{1}{2}u_1^2 + \frac{\gamma}{\gamma-1} \frac{p_1}{\rho_1} + \frac{4P_1}{\rho_1} \right) h_1\rho_1 u_1. \end{aligned} \quad (15)$$

$$\begin{aligned} \frac{h}{h_1} \frac{\rho_1}{\rho} \frac{\alpha_1}{\tau_1 \beta_1} \frac{d}{d\tilde{x}} \frac{P}{P_1} &= \frac{1}{2} \gamma \mathcal{M}_1^2 \left[\left(\frac{\rho_1}{\rho} \right)^2 \left(\frac{h_1}{h} \right)^2 - 1 \right] \\ &\quad + \frac{\gamma}{\gamma-1} \left(\frac{p}{p_1} \frac{\rho_1}{\rho} - 1 \right) + 4\alpha_1 \left(\frac{P}{P_1} \frac{\rho_1}{\rho} - 1 \right). \end{aligned} \quad (16)$$

$$20 \frac{h}{h_1} p - p_1 + \frac{h}{h_1} P - P_1 = P_1 \frac{\gamma}{\alpha_1} \mathcal{M}_1^2 \left(1 - \frac{h_1}{h} \frac{\rho_1}{\rho} \right). \quad (17)$$



3 輻射圧優勢の場合

- Overall jump conditions

- 輻射圧 P

$$\frac{4P_2}{\rho_2} - \frac{4P_1}{\rho_1} + \frac{1}{2} \frac{\frac{h_2}{h_1} P_2 - P_1}{\frac{h_2}{h_1} \rho_2 - \rho_1} \left(\frac{\rho_1}{\rho_2} \frac{h_1}{h_2} - \frac{\rho_2}{\rho_1} \frac{h_2}{h_1} \right) = 0,$$
$$\frac{h_2^2}{h_1^2} = \frac{\rho_1}{\rho_2} \frac{P_2}{P_1},$$

- 表面密度 $\Sigma = h\rho$

$$7 \frac{P_2}{\Sigma_2} h_2 - 7 + \frac{1}{\Sigma_2} - h_2 P_2 = 0,$$
$$\Sigma_2 h_2 = P_2,$$

and finally solved as

$$\Sigma_2 = \frac{1}{14} \left[1 - P_2^2 + \sqrt{(1 - P_2^2)^2 + 196 P_2^2} \right].$$





3 輻射圧優勢の場合

- Overall jump conditions

- P

- $\Sigma = h\rho$

$$(\tilde{h}_2 \tilde{P}_2 - 1) \frac{\tilde{h}_2 \tilde{\rho}_2}{\tilde{h}_2 \tilde{\rho}_2 - 1} = \frac{\gamma}{\alpha_1} \mathcal{M}_1^2,$$

where $\alpha_1 = P_1/p_1$.

$$\frac{P_2^2 - \Sigma_2}{\Sigma_2 - 1} = \frac{\gamma}{\alpha_1} \mathcal{M}_1^2.$$

$$\Sigma_2 = \frac{7(\gamma/\alpha_1) \mathcal{M}_1^2}{(\gamma/\alpha_1) \mathcal{M}_1^2 + 8},$$

$$P_2^2 = \frac{[6(\gamma/\alpha_1) \mathcal{M}_1^2 - 1](\gamma/\alpha_1) \mathcal{M}_1^2}{(\gamma/\alpha_1) \mathcal{M}_1^2 + 8},$$

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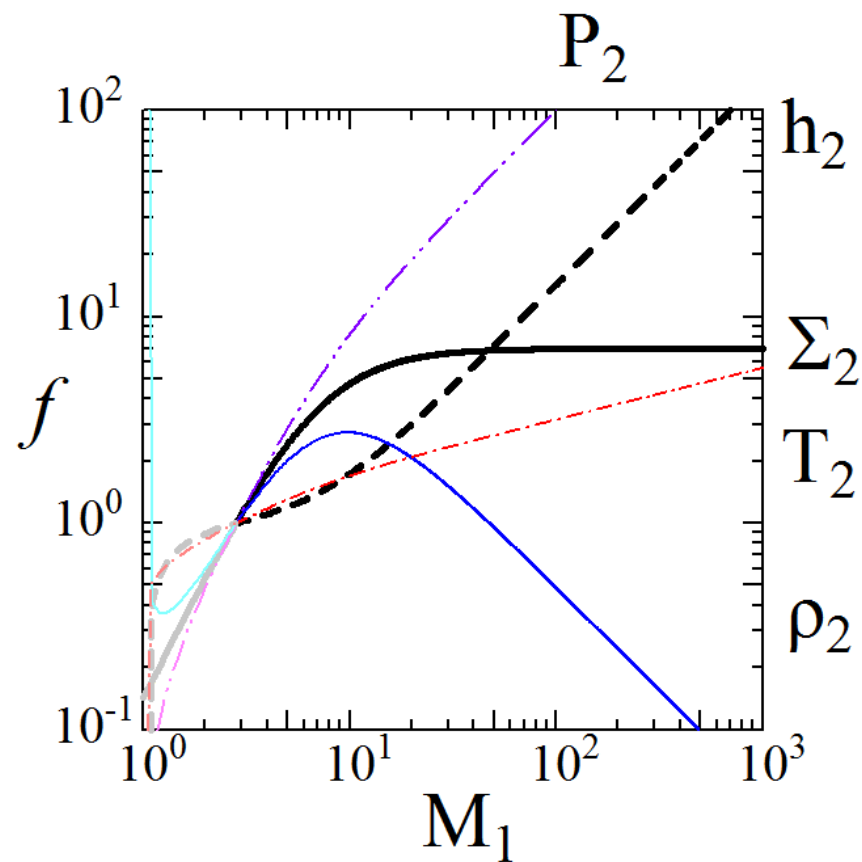
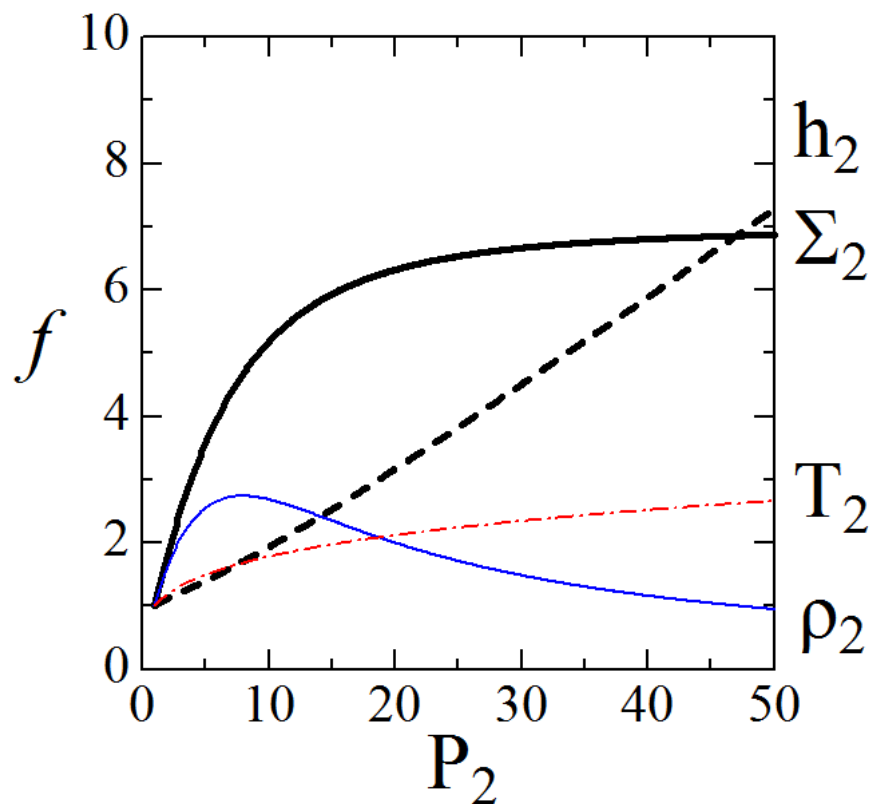




3 輻射圧優勢の場合

❁ P_2

❁ M_1





3 輻射圧優勢の場合

❁ Radiative Precursor

❁ 輻射圧 P

$$\frac{1}{\tau_1 \beta_1} \frac{\tilde{h}}{\tilde{\rho}} \frac{d\tilde{P}}{d\tilde{x}} = \frac{1}{2} \frac{\gamma}{\alpha_1} \mathcal{M}_1^2 \left(\frac{1}{\tilde{h}^2 \tilde{\rho}^2} - 1 \right) + 4 \left(\frac{\tilde{P}}{\tilde{\rho}} - 1 \right),$$
$$\tilde{h} \tilde{P} - 1 = \frac{\gamma}{\alpha_1} \mathcal{M}_1^2 \left(1 - \frac{1}{\tilde{h} \tilde{\rho}} \right),$$
$$\tilde{h}^2 = \frac{\tilde{P}}{\tilde{\rho}}.$$

Again, introducing the surface density $\Sigma (\equiv h\rho)$, and eliminating h , we can obtain the following equations:

$$\frac{1}{\tau_1 \beta_1} \frac{P^2}{\Sigma^3} \frac{dP}{dx} = \frac{1}{2} \frac{\gamma}{\alpha_1} \mathcal{M}_1^2 \left(\frac{1}{\Sigma^2} - 1 \right) + 4 \left(\frac{P^2}{\Sigma^2} - 1 \right),$$
$$\Sigma = \frac{P^2 + (\gamma/\alpha_1) \mathcal{M}_1^2}{1 + (\gamma/\alpha_1) \mathcal{M}_1^2}.$$

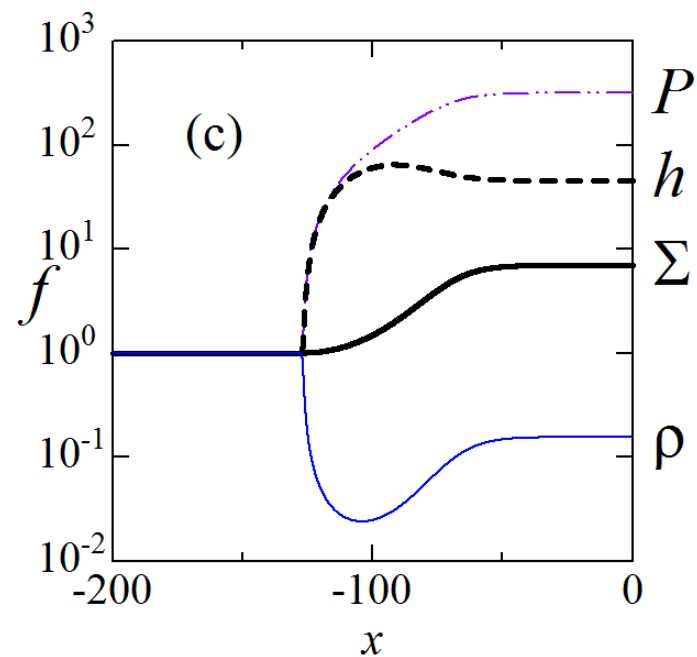
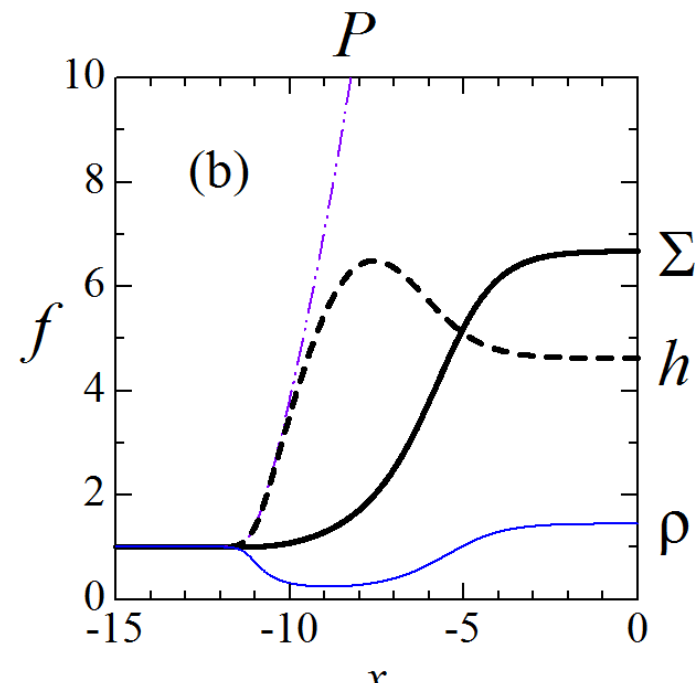
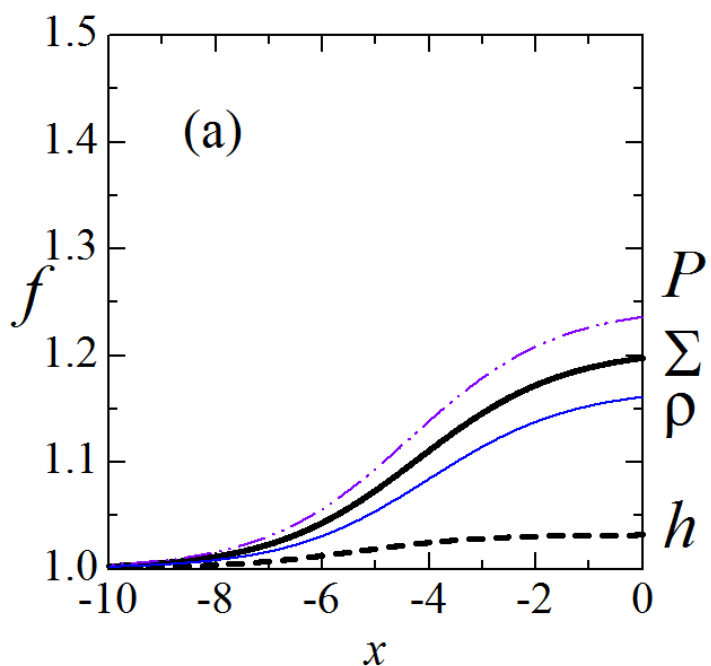




3 輻射压優勢

- ❁ Radiative Precursor
- ❁ Continuous Shock
- ❁ $\gamma=5/3$, $\alpha_1=P_1/p_1=100$
- ❁ $M_1=$
- ❁ 10,
- ❁ 100,
- ❁ 1000

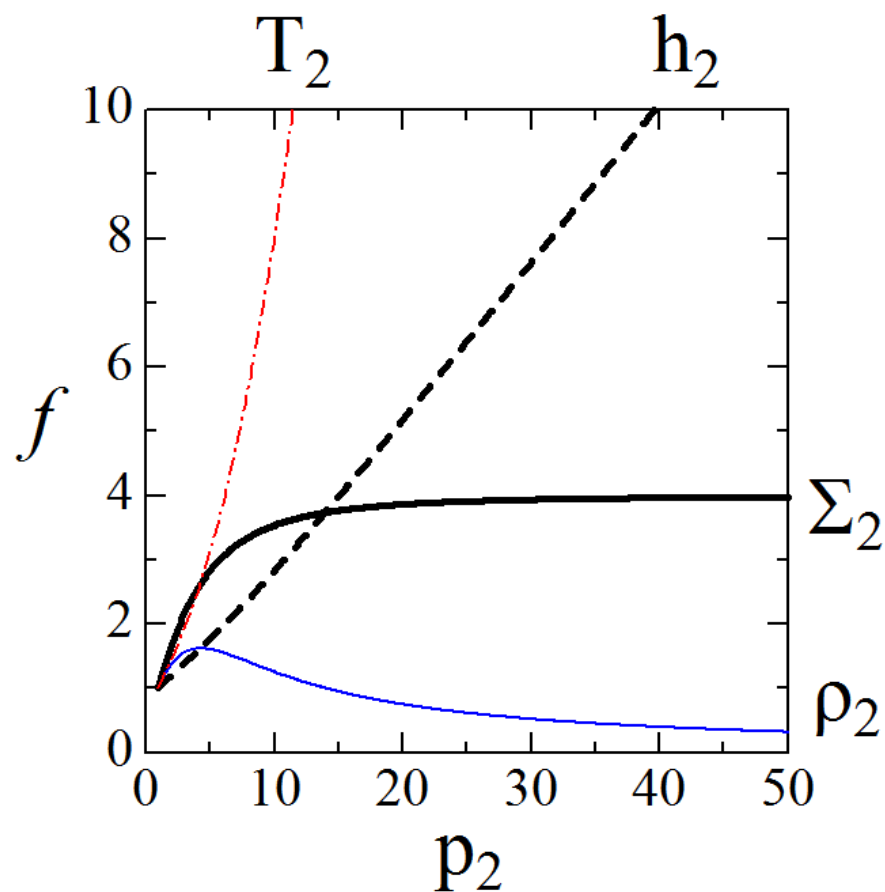
❁ Co



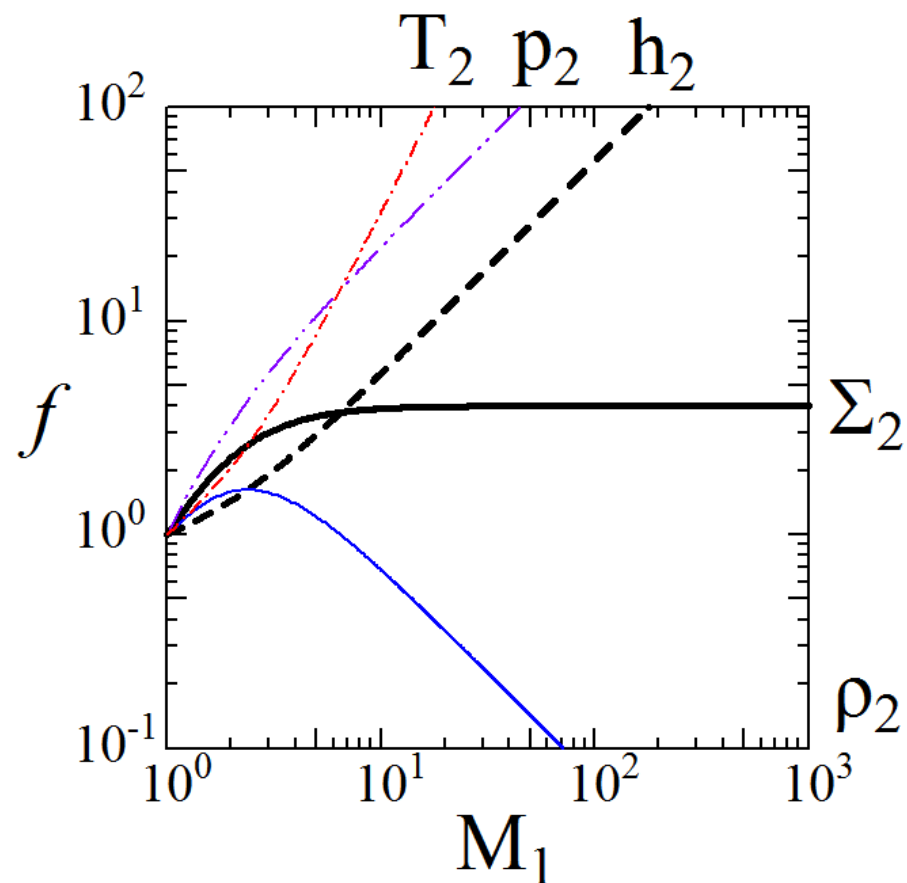


4 ガス圧優勢の場合

✿ p_2



✿ M_1





4 ガス圧優勢の場合

- ❁ Radiative Precursor

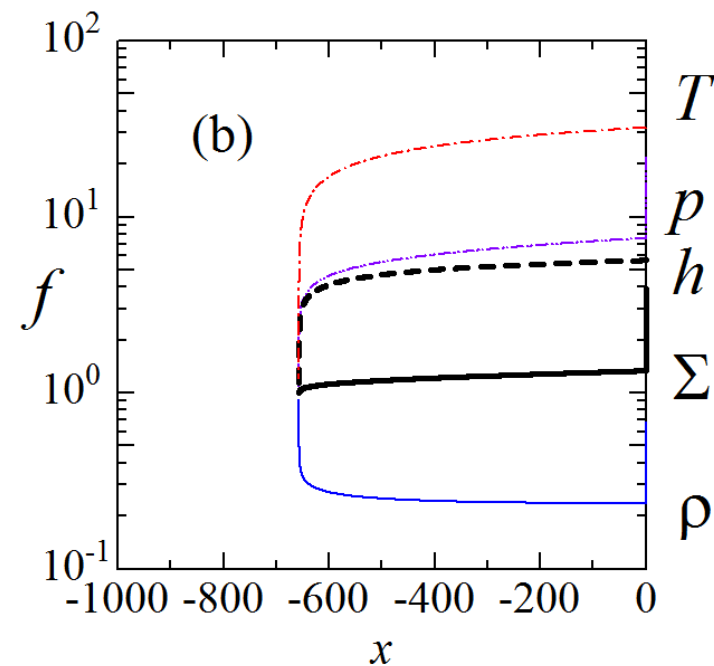
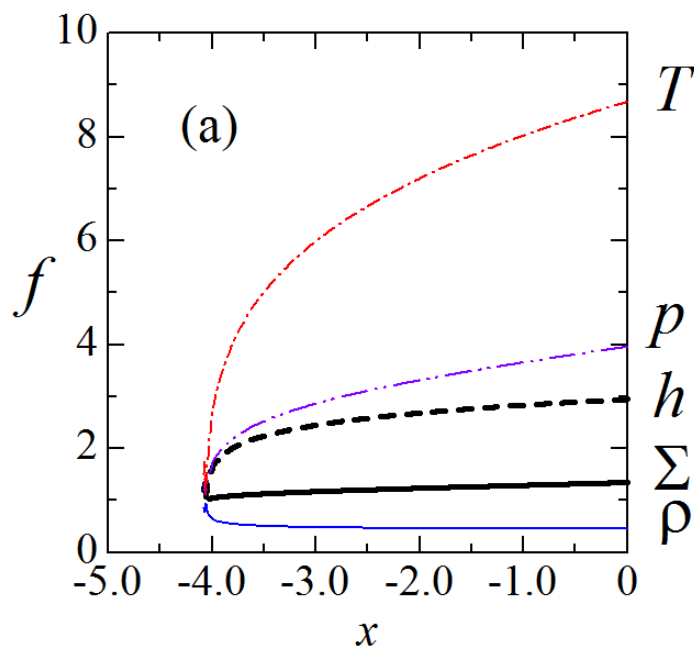
- ❁ Isothermal Shock

- ❁ $\gamma=5/3$, $\alpha_1=0.00001$

- ❁ $M_1=$

- ❁ 5

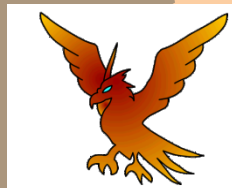
- ❁ 10





課題

- ❁ magnetic field
- ❁ gas+radiation pre.
- ❁ rigorous EoS
- ❁ 重力場、曲率変化
 - Fukue 2019d
- ❁ 遷音速解とつなげる
- ❁ wave
- ❁ stability
- ❁ multi-components
 - dust
 - pair plasma





今後の課題

- ❁ 平衡拡散近似 (1-T)
 - 非平衡拡散 (2-T)
 - 輻射輸送方程式
- ❁ 降着流への組み込み
 - Okuda+ 2004
 - 重力場の変化、角運動量保存
- ❁ 相対論的輻射性衝撃波
 - cf. Cissoko 1997; Farris+ 2008; Budnik+ 2010; Takahashi+ 2013; Sadowski+ 2013; Tolstov+ 2015; Beloborodov 2017; Fukue 2018c





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